

A MOLECULAR DYNAMICS / EXTENDED FINITE ELEMENT METHOD FOR DYNAMIC CRACK PROPAGATION

Pascal Aubertin¹, Julien Réthoré¹, and René de Borst²

¹*Université de Lyon, CNRS INSA-Lyon, LaMCoS UMR 5259, France*

²*Eindhoven University of Technology, Eindhoven, Netherlands*

Abstract. A multiscale method is presented which couples a molecular dynamics approach for describing fracture at the crack tip with an extended finite element method for discretizing the remainder of the domain. After recalling the basic equations of molecular dynamics and continuum mechanics the discretization is discussed for the continuum subdomain where the partition-of-unity property of finite element shape functions is used, since in this fashion the crack in the wake of its tip is naturally modelled as a traction-free discontinuity. Next, the zonal coupling method between the atomistic and continuum models is described, including an assessment of the energy transfer between both domains for a one-dimensional problem. Finally, a two-dimensional computation is presented of dynamic fracture using the coupled model.

Keywords. multiscale methods, molecular dynamics, extended finite element method, fracture, crack propagation

1. INTRODUCTION

Modern research into fracture commences with the seminal work of Griffith [1]. Later, Irwin [2] and Rice [3] established the relation between the stress intensity factors and the energy release rate, and gave linear elastic fracture mechanics a firm basis. However, linear elastic fracture mechanics only applies to crack-like flaws in an otherwise linear elastic solid and when the singularity associated with that flaw is characterized by a non-vanishing energy release rate. The fracture and any dissipative processes must also be confined to a small region in the vicinity of the crack tip.

When the region in which the separation and dissipative process take place is not small compared to a structural dimension, but any nonlinearity is confined to a surface emanating from a classical crack tip, i.e. one with a non-vanishing energy release rate, cohesive zone models as introduced by Barenblatt [4] and Dugdale [5] apply. The cohesive zone approach was extended by Hillerborg *et al.* [6] and Needleman [7] to circumstances where: (i) an initial crack-like flaw need not be present or, if one is present, it need not be associated with a non-vanishing energy release rate; and (ii) non-linear deformation behaviour may occur over an extended volume. Initially, cohesive-zone models were incorporated in finite element methods via special-purpose interface elements [8, 9], but more

recently, partition-of-unity finite element methods have shown to be very amenable to the incorporation of cohesive-zone models, e.g. [10–12]. In particular, they naturally enable crack *propagation*, also in dynamics [13–17] and in multi-phase continua [18, 19].

In spite of the power of the cohesive-zone approach, and its wide applicability on a range of scales, it remains a phenomenological approach. Probably, quantum mechanics is physically the most appropriate theory to describe fracture, but the difficulties to relate quantum mechanics to continuum mechanics, e.g. via Density Functional Theory [20, 21] presently seem insurmountable. One scale of observation higher is to use Molecular Dynamics to describe fracture processes from a more fundamental physics point of view. Indeed, researchers have recently used this approach to describe fracture, e.g. [22–24]. A disadvantage of the approach is that it is computationally demanding. For this reason multi-scale approaches have been introduced, in fracture [25], as well as in plasticity [26], in which only a part of the body is analysed using molecular dynamics, while the remaining part of the body is modelled using continuum mechanics and discretized using a finite element method. This manuscript furthers along this line and combines molecular dynamics for modelling the fracture process at the crack tip with an extended finite element method (XFEM), where the partition-of-unity property of the polynomial shape functions is exploited to model the crack in the wake of the tip as a traction-free discontinuity. It is noted that recently another approach has been published that couples atomistics and extended finite elements [27], but the current paper makes a further advancement in that it includes dynamic loadings.

A major issue in multi-scale approaches as discussed above is the accurate coupling of both domains, especially when different descriptions are assumed on either domain. While the coupling can, in principle, either be achieved at a discrete interface, or on a zone of a finite size (overlap or zonal coupling), it is believed that zonal approaches, which include the Arlequin method [28], the bridging domain method [29–32], discrete-to-continuum bridging [33], the discontinuous enrichment method [34], and bridging scale decomposition [35, 36] enable a more gradual transition from one domain to the other. The ability of a gradual transition is especially important for highly dissimilar domains and when wave propagation phenomena are considered, where preservation of the energy and avoiding spurious reflections when a wave exits one domain and enters the other can become an issue. Inspired by earlier work by Ben Dhia and Rateau [28] and Xiao and Belytschko [29] we have chosen a weak coupling between the models in the two adjacent domains.

This paper is organized as follows. First, we briefly list the equations of molecular dynamics. This is followed by a succinct recapitulating of the governing equations of continuum mechanics, both in the strong and the weak forms. The discretization of the continuum subdomain is carried out using the extended finite element method, where the partition-of-unity property of finite element shape functions is used to model the traction-free discontinuity in the wake of the crack tip. Subsequently, it is discussed how both domains can be coupled, see also [37] and an analysis is presented of the energy conservation properties of the coupling scheme. The paper concludes with a full two-dimensional

coupled analysis of dynamic crack propagation which shows multiple branching and suggests the formation of dislocations, which shows similarities with recent simulations on dynamic fracture using cohesive-zone models [9, 17].

2. MOLECULAR DYNAMICS

For the discrete domain, i.e. Ω_m , we build a grid of N_a atoms, and, accordingly, the initial value problem in this domain can be written as:

For $1 \leq i \leq N_a(t)$ and $t \in [0; T]$, given the initial conditions $(\mathbf{d}(0), \dot{\mathbf{d}}(0))$, find $(\mathbf{d}, \mathbf{f}) \in \mathcal{D}^{ad} \times \mathcal{F}^{ad}$ such that:

$$m_i \ddot{\mathbf{d}}_i = \mathbf{f}_i \quad (1)$$

with m_i the mass of atom i and:

$$\mathcal{D}^{ad} = \left\{ \mathbf{d} = (\mathbf{d}_i(t))_{1 \leq i \leq N_a}, \forall t \in [0, T] \right\} \quad (2)$$

$$\mathcal{F}^{ad} = \left\{ \mathbf{f} = (\mathbf{f}_i(t) = -\nabla_i \mathcal{U}(\mathbf{d}(t)))_{1 \leq i \leq N_a}, \forall t \in [0, T] \right\}$$

from where it transpires that the interatomic forces are derived from a potential energy \mathcal{U} . \mathbf{d} and \mathbf{f} assemble the discrete displacements \mathbf{d}_i and forces \mathbf{f}_i of the individual atoms, respectively. The internal energy of the discrete domain can be viewed as the sum of each atomic contribution \mathcal{U}_j :

$$\mathcal{U} = \sum_j \mathcal{U}_j(\mathbf{d}) \quad (3)$$

and the force \mathbf{f}_i acting on atom i can be written as the sum of all elementary forces:

$$\mathbf{f}_i = -\frac{\partial \mathcal{U}}{\partial \mathbf{d}_i} = \sum_{j \neq i} \mathbf{f}_{ij} \quad (4)$$

In order to limit the cost of computing such a force, we reduce the summation by only including so-called ‘‘nearest’’ neighbours, within a cut-off radius r_c :

$$\mathbf{f}_i \simeq \sum_{r_{ij} < r_c} \mathbf{f}_{ij} \quad (5)$$

where r_{ij} is the interatomic distance.

In the subdomain Ω_m the weak formulation becomes:

$$\forall \mathbf{w}^* \in \dot{\mathcal{D}}^{ad,0}, \text{ given the initial conditions } (\mathbf{d}(0), \dot{\mathbf{d}}(0)), \\ \text{find } \mathbf{d} \in \mathcal{D}^{ad} \text{ such that:}$$

$$a_m(\mathbf{d}, \mathbf{w}^*) = 0 \quad (6)$$

with \mathbf{w}^* the test function, and

$$a_m(\mathbf{d}, \mathbf{w}^*) = \sum_{i=1}^{N_a} m_i \ddot{\mathbf{d}}_i \cdot \mathbf{w}_i^* + \sum_{i=1}^{N_a} \nabla_i \mathcal{U}(\mathbf{d}) \cdot \mathbf{w}_i^*$$

3. CONTINUUM MODEL

Assuming small deformation gradients for simplicity, the governing equations in the continuum subdomain Ω_M can be written in a standard manner as:

$$\begin{aligned} \text{For } \mathbf{x} \in \Omega_M(t) \text{ and } t \in [0; T], \text{ given the initial conditions } (\mathbf{u}(\mathbf{x}, 0), \dot{\mathbf{u}}(\mathbf{x}, 0)), \\ \text{find } (\mathbf{u}, \boldsymbol{\sigma}) \in \mathcal{U}^{ad} \times \mathcal{S}^{ad} \text{ such that:} \end{aligned} \quad (7)$$

$$\rho \ddot{\mathbf{u}} = \text{div } \boldsymbol{\sigma} + \mathbf{g}_d$$

with ρ the mass density and \mathbf{u} the continuum displacement vector, $\boldsymbol{\sigma}$ the stress tensor, and \mathbf{g}_d the body force vector applied in Ω_M , subject to the boundary conditions

$$\mathcal{U}^{ad} = \left\{ \mathbf{u} = \mathbf{u}(\mathbf{x}, t) \in [\mathcal{H}^1(\Omega_M)]^3 ; \mathbf{u} = \mathbf{u}_d \text{ on } \partial_1\Omega, \forall t \in [0, T] \right\} \quad (8)$$

$$\mathcal{S}^{ad} = \left\{ \boldsymbol{\sigma} = \mathbb{K} : \nabla \mathbf{u}(\mathbf{x}, t) \in [\mathcal{L}^2(\Omega_M)]^6 ; \boldsymbol{\sigma} \cdot \mathbf{n} = \mathbf{F}_d \text{ on } \partial_2\Omega, \forall t \in [0, T] \right\}$$

where \mathbb{K} is the fourth-order stiffness tensor, \mathbf{n} the outward normal vector to $\partial\Omega_2$, and \mathbf{u}_d and \mathbf{F}_d the prescribed displacements and tractions at $\partial\Omega_1$ and $\partial\Omega_2$, respectively.

To allow for a discretization of the continuum subdomain we next specify the weak formulation:

$$\begin{aligned} \forall \mathbf{v}^* \in \dot{\mathcal{U}}^{ad,0}, \text{ given the initial conditions } (\mathbf{u}(\mathbf{x}, 0), \dot{\mathbf{u}}(\mathbf{x}, 0)), \\ \text{find } \mathbf{u} \in \mathcal{U}^{ad} \text{ such that:} \\ a_M(\mathbf{u}, \mathbf{v}^*) = l_M(\mathbf{v}^*) \end{aligned} \quad (9)$$

with \mathbf{v}^* the test function, and

$$a_M(\mathbf{u}, \mathbf{v}^*) = \int_{\Omega_M} \rho \ddot{\mathbf{u}} \cdot \mathbf{v}^* d\Omega + \int_{\Omega_M} \boldsymbol{\epsilon}(\mathbf{u}) : \mathbb{K} : \boldsymbol{\epsilon}(\mathbf{v}^*) d\Omega \quad (10)$$

$$l_M(\mathbf{v}^*) = \int_{\partial_2\Omega} \mathbf{F}_d \cdot \mathbf{v}^* dS + \int_{\Omega_M} \mathbf{g}_d \cdot \mathbf{v}^* d\Omega \quad (11)$$

4. COUPLING SCHEME

4.1. Coupling functions

In order to enable an efficient coupling between the two domains, a coupling zone is defined and a coupling function is computed which is used to obtain the global energy. First a coupling length L_c is chosen such that will be the characteristic length of the coupling region. Subsequently, the patch of atoms, Ω_m , is included in the continuum at a given position. Atoms at a distance $\ell \leq L_c$ from the Molecular Dynamics Box (MD-Box) boundary are considered to be in the coupling zone Ω_c . The finite elements in this zone are named ‘‘coupling elements’’. Inside the MD-Box, where only the atomistic model applies, elements are removed. The resulting, discretized domain is shown in Figure 1. In principle, each atom must be coupled to the finite element discretization of the underlying continuum. It suffices to couple only a limited number of atoms to the underlying continuum without loss of accuracy. Since this directly affects the size of the coupling matrices that

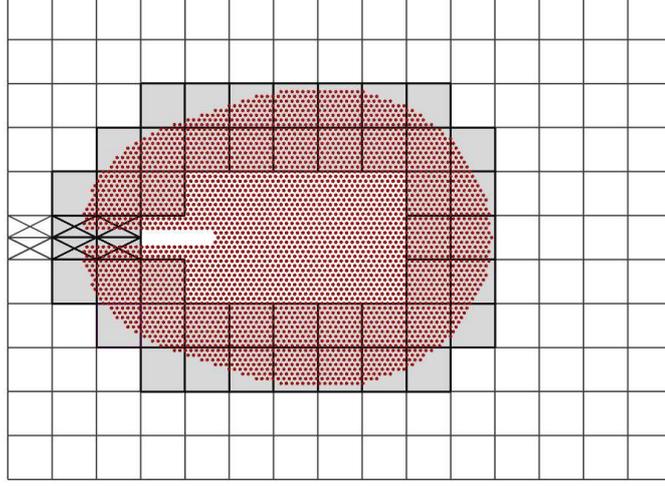


Fig. 1. Discretized domain with the coupling region. The dark, “pear-shaped” area is the domain where an MD calculation is carried out (Ω_m). The coupling region Ω_c consists of elements that are surrounded by a bold line

will be derived next, such a limited coupling markedly decreases the computational effort, and therefore, a bigger scale transition becomes possible at reasonable computational costs.

In the coupling zone Ω_c , we enforce a velocity coupling in a weak sense, and we distribute the energy between both models via a partition of unity [28]. For this purpose we define the following functions, see Figure 2:

$$\alpha : \Omega_M \rightarrow [0, 1] \quad (12)$$

$$\beta : \Omega_m \rightarrow [0, 1] \quad (13)$$

such that:

$$\begin{cases} \alpha(\mathbf{x}) = 1 & \text{for } \mathbf{x} \in \Omega_M \setminus \Omega_c \\ \beta(\mathbf{x}) = 1 & \text{for } \mathbf{x} \in \Omega_m \setminus \Omega_c \\ \alpha(\mathbf{x}) + \beta(\mathbf{x}) = 1 & \text{for } \mathbf{x} \in \Omega_c \end{cases} \quad (14)$$

The displacement and velocity fields in the domains Ω_M and Ω_m have a different nature. In Ω_M we have a continuum field, while in Ω_m we have a discrete field, which is only defined at the geometrical points corresponding to the atoms. Therefore we construct a so-called “mediator space”, denoted by \mathcal{M} , on which we project the fields $\dot{\mathbf{u}}$ and $\dot{\mathbf{d}}$ in order to be able to compare them. The nature of \mathcal{M} is constrained by the discrete character of the atomistic field. Indeed, its displacements cannot be extrapolated outside the atomic positions if we want to maintain a physical interpretation at the fine scale. Accordingly, \mathcal{M} has to be a subspace of the physical atomistic space. More precisely, we project the velocities using an operator Π on a discrete subset $\overline{\Omega}_c$ of the atomic positions included in

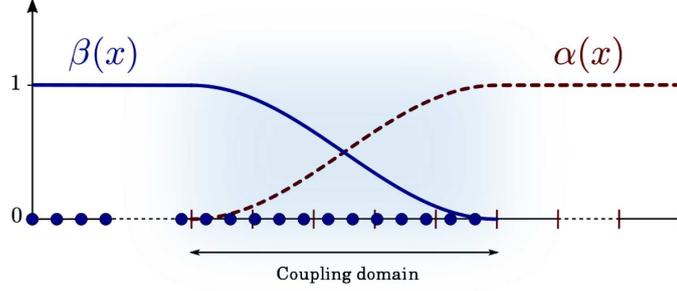


Fig. 2. Partition of unity for the energy distribution

Ω_c . Considering that \mathcal{M} is built as a Hilbert space, we introduce a scalar product c from $\mathcal{M} \times \mathcal{M}$ onto \mathbb{R} . With these definitions we formulate the velocity coupling operator as:

$$\forall \mu^* \in \mathcal{M} \quad , \quad c(\mu^*, \Pi \dot{\mathbf{u}} - \Pi \dot{\mathbf{d}}) = \langle \mu^*, \Pi \dot{\mathbf{u}} - \Pi \dot{\mathbf{d}} \rangle_{\mathcal{M}} \quad (15)$$

with c the classical scalar product on \mathcal{M} . The global equations are coupled via Lagrange multipliers and can subsequently be written as:

$$\begin{aligned} \forall (\mathbf{v}^*, \mathbf{w}^*, \boldsymbol{\mu}^*) &\in \dot{\mathcal{U}}^{ad,0} \times \dot{\mathcal{D}}^{ad,0} \times \mathcal{M}, \\ \text{given the initial conditions } &(\mathbf{u}(\mathbf{x}, 0), \dot{\mathbf{u}}(\mathbf{x}, 0), \mathbf{d}(0), \dot{\mathbf{d}}(0)), \\ \text{find } (\mathbf{u}, \mathbf{d}, \boldsymbol{\lambda}) &\in \mathcal{U}^{ad} \times \mathcal{D}^{ad} \times \mathcal{M} \text{ such that:} \end{aligned}$$

$$a_{\alpha,M}(\mathbf{u}, \mathbf{v}^*) + a_{\beta,m}(\mathbf{d}, \mathbf{w}^*) + c(\boldsymbol{\lambda}, \Pi \mathbf{v}^* - \Pi \mathbf{w}^*) + c(\boldsymbol{\mu}^*, \Pi \dot{\mathbf{u}} - \Pi \dot{\mathbf{d}}) = l_{\alpha,M}(\mathbf{v}^*) \quad (16)$$

The modified forms $a_{\alpha,M}$, $a_{\beta,m}$ and $l_{\alpha,M}$ take into account the weighting functions $\alpha(\mathbf{x})$ and $\beta(\mathbf{x})$, see [37] for details. In the atomistic subdomain the modified form $a_{\beta,m}$ that takes into account the distribution of the energy reads:

$$a_{\beta,m}(\mathbf{d}, \mathbf{w}^*) = \mathbf{w}^* \cdot \mathbf{m}_\beta \ddot{\mathbf{d}} - \mathbf{w}^* \cdot \mathbf{f}_\beta \quad (17)$$

with:

$$\beta_i = \beta(\mathbf{d}_i) \quad , \quad \mathbf{m}_\beta = [\beta_i \delta_{i,j} m_i] \quad , \quad \mathbf{f}_\beta = [\mathbf{f}_{\beta,i}] \quad (18)$$

4.2. Discretized problem

In a manner which is by now standard the interpolation of each component of the displacement field is enriched with discontinuous functions in order to properly capture the traction-free discontinuity in the wake of the crack tip:

$$\forall \mathbf{x} \in \Omega_M \quad , \quad u_h(\mathbf{x}) = \sum_{i \in \mathcal{N}_M} N_i(\mathbf{x}) \bar{u}_i + \sum_{i \in \mathcal{N}_{cut}} N_i(\mathbf{x}) \mathcal{H}_{\Gamma_d} \hat{u}_i \quad (19)$$

where N_i are standard finite element shape functions supported by the set of nodes \mathcal{N}_M included in the discretized domain Ω_M . Nodes in \mathcal{N}_{cut} have their support cut by the discontinuity. They hold additional degrees of freedom \hat{u}_i corresponding to the discontinuous function \mathcal{H}_{Γ_d} defined by:

$$\mathcal{H}_{\Gamma_d}(\mathbf{x}) = \frac{\mathbf{x} \cdot \mathbf{n}_{\Gamma_d}}{\|\mathbf{x} \cdot \mathbf{n}_{\Gamma_d}\|} \quad (20)$$

with \mathbf{n}_{Γ_d} the normal to the discontinuity Γ . Symbolically, eq. (19) can be written as

$$\forall \mathbf{x} \in \Omega_M \quad , \quad \mathbf{u}_h = \mathbf{N}^T \mathbf{U} \quad (21)$$

where the matrix \mathbf{N} contains the standard interpolation polynomials $N_i(\mathbf{x})$ as well as the discontinuous function \mathcal{H}_{Γ_d} , and the array \mathbf{U} contains the displacement degrees-of-freedom \bar{u}_i and \hat{u}_i . The transition within the domain Ω_M between the subdomain where the nodes are “enriched” and the part which has just the standard formulation does not affect the Molecular Dynamics computation other than through the coupling matrices.

With the latter symbolic notation the bilinear form $a_{\alpha,M}$ and the linear form $l_{\alpha,M}$ become:

$$a_{\alpha,M}(\mathbf{u}_h, \mathbf{v}_h^*) = \mathbf{V}^{*T} \mathbf{M}_\alpha \ddot{\mathbf{U}} + \mathbf{V}^{*T} \mathbf{K}_\alpha \mathbf{U} \quad (22)$$

$$l_{\alpha,M}(\mathbf{v}_h^*) = \mathbf{V}^{*T} \mathbf{F}_\alpha \quad (23)$$

where the term that represents the body forces has been omitted for simplicity, and

$$\mathbf{M} = \int_{\Omega_M} \rho \mathbf{N}^T \mathbf{N} d\Omega \quad (24)$$

$$\mathbf{K} = \int_{\Omega_M} \nabla \mathbf{N}^T \mathbb{K} \nabla \mathbf{N} d\Omega \quad (25)$$

the mass and stiffness matrices, respectively. With the standard definition of the scalar product, the coupling term in the continuum can be discretized as follows:

$$c(\boldsymbol{\lambda}, \Pi \mathbf{v}_h^*) = \mathbf{V}^{*T} \mathbf{C}_M \boldsymbol{\Lambda} = \mathbf{V}^{*T} \mathbf{F}_M^L \quad (26)$$

with \mathbf{C}_M the continuum coupling matrix. The vector $\boldsymbol{\Lambda}$ contains the Lagrange multipliers and its size equals the $\bar{\Omega}_c$ subset cardinal times the dimension of the space considered. \mathbf{F}_M^L can be regarded as a fictitious force due to the coupling via the Lagrange multipliers. This force has a non-zero value only in the coupling zone Ω_c .

Using the Lagrange multipliers in the atomistic domain similar to that in the continuum domain:

$$\mathbf{f}_m^L = \mathbf{C}_m \boldsymbol{\Lambda} \quad (27)$$

the weighted and coupled system (16) can be cast in a matrix-vector format:

$$\begin{aligned} \mathbf{V}^{*T} (\mathbf{M}_\alpha \ddot{\mathbf{U}} + \mathbf{K}_\alpha \mathbf{U} + \mathbf{C}_M \boldsymbol{\Lambda}) + \mathbf{W}^{*T} (\mathbf{m}_\beta \ddot{\mathbf{d}} - \mathbf{f}_\beta - \mathbf{C}_m \boldsymbol{\Lambda}) + \\ \boldsymbol{\mu}^{*T} (\mathbf{C}_M^T \dot{\mathbf{U}} - \mathbf{C}_m^T \dot{\mathbf{d}}) = \mathbf{V}^{*T} \mathbf{F}_\alpha \end{aligned} \quad (28)$$

Since this set must hold for any admissible $(\mathbf{V}^*, \mathbf{W}^*, \boldsymbol{\mu}^*)$ we finally obtain:

$$\begin{cases} \mathbf{M}_\alpha \ddot{\mathbf{U}} + \mathbf{K}_\alpha \mathbf{U} = \mathbf{F}_\alpha - \mathbf{C}_M \boldsymbol{\Lambda} \\ \mathbf{m}_\beta \ddot{\mathbf{d}} = \mathbf{f}_\beta + \mathbf{C}_m \boldsymbol{\Lambda} \\ \mathbf{C}_M^T \dot{\mathbf{U}} = \mathbf{C}_m^T \dot{\mathbf{d}} \end{cases} \quad (29)$$

with $(\mathbf{U}, \mathbf{d}, \boldsymbol{\Lambda})$ the set of unknowns. Details on the time integration scheme associated with this set of coupled ordinary differential equations are given in Ref. [37].

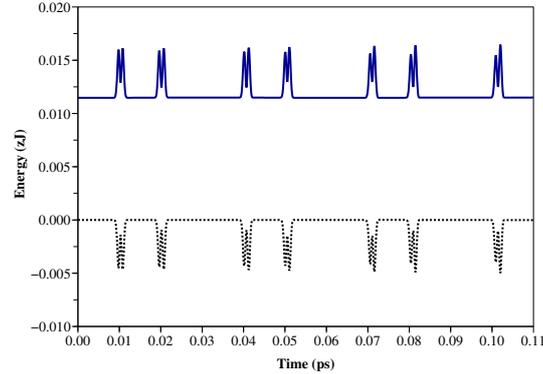


Fig. 3. Mechanical energy (drawn line) and the work stored in the Lagrange multipliers (dashed line) when the prediction step is with the full stiffness and mass matrices.

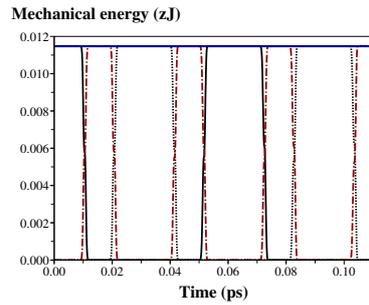
4.3. Energy transfer between the atomistics and continuum domains

The energy transfer for the coupling between the continuum and atomistic domains is studied by means of a longitudinal bar discretized with finite elements, and containing an atomistic region, with a coupling zone on both sides. The bar is submitted to a traction wave, which is enforced by displacing the left-most 20 elements in the initial configuration. The right-hand end is free. The whole domain is $59.142528 \times 10^{-9} m$ long and 100 atoms have been put in the atomistic domain. The interatomic distance is $r_e = 0.1234708 \times 10^{-9} m$, and the finite element size is $h = r_e$. We use a Lennard-Jones potential as constitutive model for the atoms, with $a = 32.043529 \times 10^{-21} J$ and a mass $m = 0.0016599 \times 10^{-24} g$. The elastic material properties for the finite element model have been derived from the atomic properties [39]. The computation continues for 2000 time steps with $\Delta t = 1 \times 10^{-15} s$, which amounts to 95% of the critical time step.

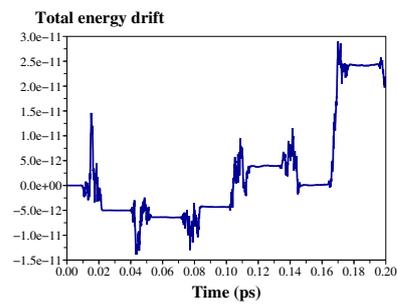
Figure 3 shows the total mechanical energy during the computation. We observe some fluctuations each time the wave crosses a coupling zone. In fact, work is stored by the Lagrange multipliers, and subsequently put back in the mechanical system when the wave exits the coupling zone. We observe that the work of the Lagrange multipliers is complementary to the mechanical energy, and the energy balance is therefore satisfied. From energy plots of Figure 4 we observe that for different coupling lengths (i) the total energy is preserved, and that (ii) the energy correctly passes from one domain to the other when the wave traverses the coupling zones.

5. DYNAMIC FRACTURE

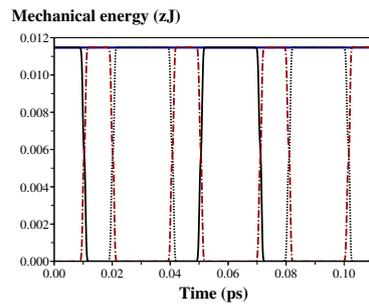
We now proceed with a two-dimensional simulation of dynamic fracture. A copper single crystal is considered in its (111) plane, so that the two-dimensional lattice is hexagonal. The Lennard-Jones potential is used in the molecular dynamics simulation with parameters from [38]: $a = 0.415 eV$ and $b = 0.2277 nm$. The Young's modulus E



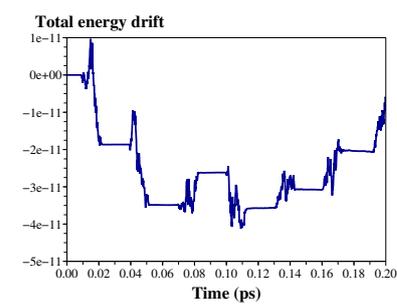
(a) Energy transfer for L_c consisting of 2 elements



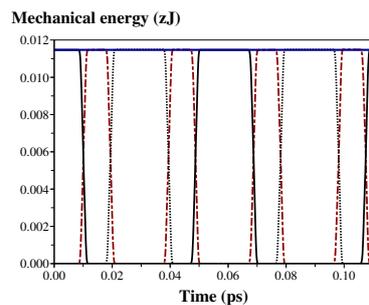
(b) Energy drift for L_c consisting of 2 elements



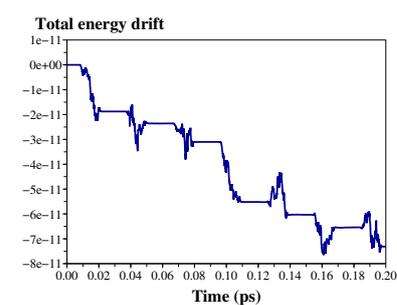
(c) Energy transfer for L_c consisting of 5 elements



(d) Energy drift for L_c consisting of 5 elements



(e) Energy transfer for L_c consisting of 10 elements



(f) Energy drift for L_c consisting of 10 elements

Fig. 4. Energy plots for the finite element - Molecular Dynamics coupling. In subfigures (a), (c) and (e) the drawn line is the energy in the first (left) continuum, the dashed line is the energy in the second (right) continuum, and the dash-dotted line represents the energy stored in the atoms. The bold drawn line is the total mechanical energy.

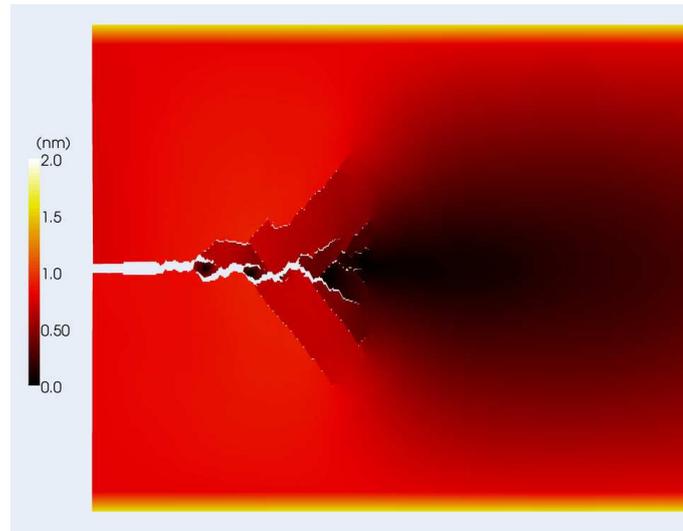


Fig. 5. Deformed configuration at $t = 33.209 \text{ ps}$

and Poisson's ratio ν for the continuum are obtained following the procedure given in [39]: $E = 79.334 \text{ GPa}$ and $\nu = 0.25$. The copper atomic mass is taken as $m = 0.105520602596 \times 10^{-24} \text{ kg}$ ($m_{Cu} = \frac{63.546}{N_A} \text{ g}$ with N_A the Avogadro number: $N_A = 6.02214179 \times 10^{23} \text{ mol}^{-1}$), which corresponds to a mass density $\rho = 1865.250812586 \times 10^3 \text{ kgm}^{-3}$. In the present study, the temperature has not been taken into account, since the focus is on the coupling of Molecular Dynamics to an (extended) finite element method for crack propagation. When extending the methodology to explicitly include the temperature a "thermal equilibrium" has to be achieved in addition to the mechanical equilibrium. This can for instance be done using the Nose-Hoover thermostat method [40].

The computational domain is 100 nm long and 77.5 nm wide with an initial crack of 10 nm . The finite element mesh consists of 1221 quadrilateral elements and 4868 nodes. The element size is about 10 times the interatomic distance. 36635 atoms are put in the vicinity of the crack tip. The width of the coupling domain is approximately 3 nm and 33% of the atoms in this region hold Lagrange multipliers. For computational reasons, the results that are presented from now on have been obtained by only including the first neighbours in the atomistic interactions. Indeed, the equilibration techniques and the updates are expensive when we take into account many neighbours. Simulations on a smaller scale have indicated that the results are close to those obtained with more neighbours.

The test consists of applying a velocity on the top and bottom edges of the specimen. The prescribed velocity in this example is $V_p = 47.4 \text{ ms}^{-1}$. The time step is 15.811388 fs (10^{-15} s). Figure 5 gives the displacement field after the crack has propagated, at $t = 33.209 \text{ ps}$. Close inspection reveals that, going from the atomistic zone to the continuum domain, no spurious wave reflections occur, which indicates that the coupling algorithm works properly, and is in agreement with results for linear elasticity presented in [37]. We

also see that, even though the prescribed loading corresponds to Mode-I and the atomistic lattice is a perfect single crystal, the crack path is not that which we would expect to obtain with classical continuum methods. We observe crack branching, the occurrence of dislocations, and locally, mixed-mode behaviour.

6. CONCLUDING REMARKS

A numerical approach has been proposed for combining a molecular dynamics method and a finite element method that exploits the partition-of-unity property of finite element shape functions (extended finite element method). The aim is to simulate dynamic fracture in an efficient manner on basis of elementary physical principles. To this end the zone around the crack tip is modelled using molecular dynamics. Around this so-called Molecular Dynamics Box a continuum mechanics approach is adopted, with the finite element method used for discretization. The partition-of-unity property of the finite element shape functions is exploited to model the crack in the wake of its tip as a traction-free discontinuity. The coupling between the continuum and molecular dynamics zones has a zonal character where the energy is partitioned over both models and a weak velocity coupling is enforced. In this manner, spurious reflections are avoided and energy is conserved when a wave travels from one zone into another.

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ĐỘNG LỰC HỌC PHÂN TỬ/ PHƯƠNG PHÁP PHẦN TỬ HỮU HẠN CHO BÀI TOÁN PHÁT TRIỂN VẾT NỨT ĐỘNG

Phương pháp đa tỷ lệ được trình bày ở đây là sự kết hợp giữa phương pháp động lực học phân tử cho việc mô tả sự phá hủy tại đỉnh của vết nứt với phương pháp phần tử hữu hạn mở rộng cho việc số hóa miền còn lại. Sau khi sử dụng các phương trình cơ bản của động lực học phân tử và cơ học môi trường liên tục, việc số hóa sẽ được thực hiện cho miền con liên tục mà ở đó tính chất phân vùng đơn vị của các hàm dạng của phần tử hữu hạn sẽ được sử dụng, do ở dạng này vết nứt trong đường lằn của đỉnh của nó sẽ được mô hình như sự không liên tục không có lực kéo. Tiếp theo, phương pháp kết hợp vùng giữa các mô hình nguyên tử và liên tục sẽ được mô tả, bao gồm việc đánh giá sự truyền năng lượng giữa hai miền cho bài toán một chiều. Cuối cùng, tính toán hai chiều cho bài toán phá hủy động lực học sử dụng mô hình kết hợp sẽ được trình bày. Từ khóa : Phương pháp đa tỷ lệ, phương pháp động lực học phân tử, phương pháp phần tử hữu hạn mở rộng, cơ học phá hủy, phát triển vết nứt